

# THE SODIUM-POTASSIUM EXCHANGE PUMP

## II. ANALYSIS OF

### Na<sup>+</sup>-LOADED FROG SARTORIUS MUSCLE

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**ABSTRACT** A model for the Na-K exchange pump was applied to data on Na<sup>+</sup>-loaded frog sartorius muscle, and was used to relate the rate of adenosine triphosphate (ATP) hydrolysis to the electrical properties of the cell membrane. Membrane hyperpolarization was considered to arise from an electrical current which was produced by the hydrolysis reaction coupled to ion movements, and which flowed across the membrane. The reaction rate, as calculated from hyperpolarization, agreed with direct measurements of ATP hydrolysis and with the rate estimated from Na<sup>+</sup> tracer efflux studies. Although Na<sup>+</sup> is actively extruded, the model showed that K<sup>+</sup> is inwardly transported if the potassium permeability of the membrane is less than about  $6.6 \times 10^{-6}$  cm/sec, as is suggested by resistance data. Calculations indicated that the reaction conductance  $L_{rr}$  was relatively constant when compared with the reaction rate and reaction free energy for large changes in internal and external ionic concentrations. Its value agreed with the value obtained from the dependence of Na<sup>+</sup> tracer efflux on external K<sup>+</sup>. A set of experiments was suggested which would provide a more complete interpretation of the data.

## INTRODUCTION

A model of the Na-K exchange pump in which membrane potential is regulated by the reaction rate of the pump, and the rate in turn depends on membrane potential, was developed in part I of this study (Rapoport, 1970) and is summarized in the Appendix. The model will be employed to analyze data on frog sartorius muscle, and the extent of its applicability and limitations will be discussed.

Keynes (1954) proposed that the increase of Na<sup>+</sup> tracer efflux in frog sartorius, when the external K<sup>+</sup> was increased, was due to a coupled Na-K exchange pump. He defined the pump as "electrogenic" when membrane potential (inside-outside) was more negative (hyperpolarized) than the K<sup>+</sup> equilibrium potential. This occurs in Na<sup>+</sup>-loaded frog sartorius muscle in 10 mM K<sup>+</sup> Ringer (Stephenson, 1953; Kernan, 1962; Mullins and Awad, 1965; Adrian and Slayman, 1966; Cross et al., 1965). The latter authors, who measured ionic concentrations and membrane po-

tentials with time in the Na<sup>+</sup>-loaded muscles, did not propose a general formulation to interpret their results. Alternatively, rather than being due directly to the electrogenic pump, the hyperpolarization in Na<sup>+</sup>-loaded muscles could be caused by K<sup>+</sup> being pumped into the muscle faster than it was replenished in the extracellular space by diffusion from the bathing solution (cf. Page and Storm, 1965; Adrian and Slayman, 1966).

The model will be used to show that in Na<sup>+</sup>-loaded muscle, membrane hyperpolarization, which we define as the difference between the membrane potential and the "diffusion" potential, can be ascribed to the electrogenic pump. Reaction rate  $J_r$ , reaction conductance  $L_r$ , the driving force on the reaction  $\Delta F_r$ , membrane resistance, and other parameters will be calculated.  $J_r$  and  $L_r$  will be shown to agree with values found by other means, and their relation to changes in internal and external concentrations will be considered.

A similar theoretical approach to Na<sup>+</sup>-loaded frog sartorius has been made by Frumento (1965), but he did not account for the dependence of the pump on membrane potential and did not propose a feedback relation between pump rate and membrane potential.

## METHODS

### *Assumed Parameters and Given Conditions*

Cross et al. (1965) exposed pairs of frog sartorius muscles at 2°C to a K<sup>+</sup>-free soaking-in solution which consisted of 89 mM NaCl, 25 mM NaHCO<sub>3</sub>, 3 mM NaH<sub>2</sub>PO<sub>4</sub>, 0.9 mM CaCl<sub>2</sub>, 1.5 mM MgSO<sub>4</sub>, equilibrated with 5% CO<sub>2</sub>-95% O<sub>2</sub>. In this solution, the Na<sup>+</sup> content of the muscles increased and the K<sup>+</sup> content decreased; the muscles became "Na<sup>+</sup>-loaded". After soaking, one muscle was transferred to a recovery solution containing 10 mM K<sup>+</sup> (Table I) and the K<sup>+</sup> and Na<sup>+</sup> contents of the other determined by flame photometry. In the recovery solution, the membrane potential of the one muscle was measured over a 1 hr period, after which its K<sup>+</sup> and Na<sup>+</sup> contents were measured. The combined values of  $\phi_s$  and  $\phi_K = RT/F \ln C_K^i/C_K^o$  (K<sup>+</sup> equilibrium potential, where superscripts 1 and 2 denote bathing solution and inside, respectively) initially and after 1 hr in recovery solution are listed in Table I for the muscle pairs, which were rank-ordered from 1 to 36 as a function of the initial potential differences  $\phi_s - \phi_K$ .

We assume that inside concentrations  $C_i^s$  change exponentially with a time constant  $\tau$  of 30 min (Desmedt, 1953; Cross et al., 1965). If the initial concentration is  $(C_i^s)_{t=0}$  and the final concentration is  $(C_i^s)_{t=\infty}$ , then

$$(C_i^s)_t = (C_i^s)_{t=\infty} + ([C_i^s]_{t=0} - [C_i^s]_{t=\infty}) \exp(-t/\tau). \quad (1a)$$

Differentiating to obtain  $dC_i^s/dt$  and noting that the volume to surface ratio of the muscle cylinder is  $r/2$  (where  $r$  is the fiber radius), the net flux of substance  $i$  per cm<sup>2</sup> surface is given by

$$J_{\text{net}, i} = (r/2\tau)([C_i^s]_{t=\infty} - [C_i^s]_{t=0}) \exp(-t/\tau). \quad (1b)$$

TABLE I  
A COMPARISON OF  $\phi_s$  AND  $\phi_K$  AT THE BEGINNING AND  
AFTER 1 HR OF RECOVERY\*

Muscle No.	Initial			1 hr		
	$\phi_s$	$\phi_K$	$\phi_s - \phi_K$	$\phi_s$	$\phi_K$	$\phi_s - \phi_K$
	<i>mv</i>	<i>mv</i>	<i>mv</i>	<i>mv</i>	<i>mv</i>	<i>mv</i>
1	-67	-49	-18	-67	-65	-2
2	-76	-60	-16	-62	-65	3
3	-43	-27	-16	-70	-60	-10
4	-55	-40	-15	-60	-59	-1
5	-72	-58	-14	-65	-68	3
6	-70	-59	-11	-65	-67	2
7	-69	-60	-9	-54	-68	14
8	-68	-60	-8	-67	-68	1
9	-68	-61	-7	-66	-66	0
10	-62	-56	-6	-61	-63	2
11	-64	-59	-5	-66	-64	-2
12	-58	-53	-5	-65	-67	2
13	-65	-61	-4	-66	-66	0
14	-52	-48	-4	-57	-63	6
15	-63	-60	-3	-63	-67	4
16	-51	-48	-3	-70	-62	-8
17	-60	-59	-1	-53	-66	13
18	-24	-27	3	-44	-55	11
19	-44	-48	4	-53	-64	11
20	-28	-34	6	-60	-61	1
21	-43	-50	7	-64	-65	1
22	-40	-47	7	-60	-68	8
23	-39	-47	8	-50	-60	10
24	-39	-48	9	-57	-59	2
25	2	-8	10	-49	-49	0
26	-32	-43	11	-49	-58	9
27	-28	-43	15	-48	-59	11
28	-28	-43	15	-50	-61	11
29	-13	-28	15	-19	-57	38
30	-19	-37	18	-40	-51	11
31	-29	-50	21	-44	-61	17
32	-26	-49	23	-50	-68	18
33	-22	-47	25	-39	-64	25
34	-22	-49	27	-33	-60	27
35	-22	-50	28	-34	-62	28
36	-17	-54	37	-42	-65	23

$C'_K = 10$  mM;  $C'_{Na} = 104$  mM;  $C'_{Cl} = 85$  mM.

$C^s_{Na}$  (initial) = 97 mM;  $C^s_{Na}$  (1 hr) = 43.3 mM.

\* From Cross et al., 1965.

The  $Na^+$  content of the individual muscles was not reported. The reported mean initial  $Na^+$  content was 80.5 mM  $Na^+$ /kg wet weight (measured on muscle in  $K^+$ -free soaking-in solution) and 38.8 mM/kg wet weight after 90 min in recovery solution. Respective mean water contents were 799 and 784 ml/kg wet weight. Fiber water and  $Na^+$  concentration/liter

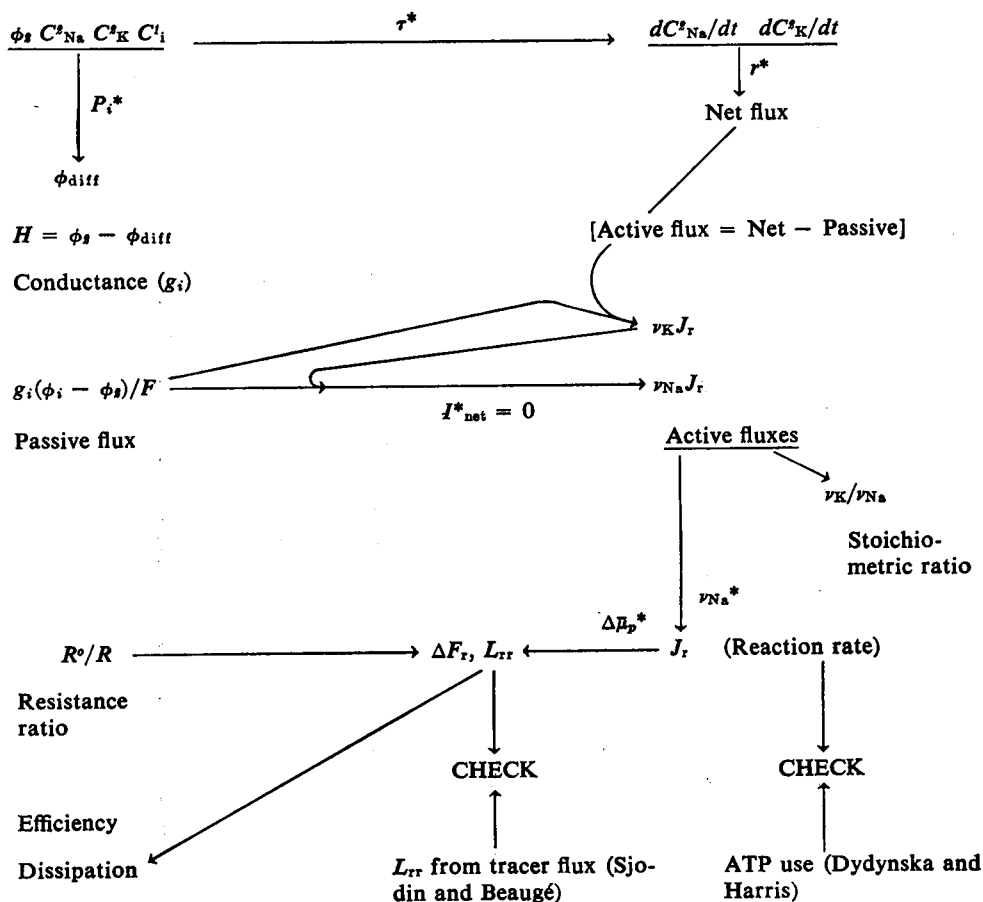


FIGURE 1 Flow chart for analysis of data on Na<sup>+</sup>-loaded frog sartorius in 10 mM K<sup>+</sup> Ringer (Cross et al., 1965). Given quantities are on first line at left. Arrows point to calculated quantities. (\*) indicates additional parameters required for calculation. CHECK shows quantities that can be compared with other data. For example, the reaction rate  $J_r$  calculated by the model can be compared with the rate of ATP hydrolysis as found by Dydyńska and Harris (1966).

fiber water were calculated as shown by Cross et al. (1965), using an extracellular space of 130 ml/kg wet weight. With use of equation 1 *a* and the values above, average internal sodium concentration was  $C_{Na}^i = 97$  mM initially and 43.3 mM at 1 hr.

Table I lists the concentrations and potentials for the initial and 1 hr conditions of Cross et al. (1965). Fiber radius  $r$  was taken as 40  $\mu$ . Although calculations require a choice of  $P_K$ , its exact value is not known. It may be constant, a function of only membrane potential, or of the difference  $\phi_s - \phi_K$  (Hodgkin and Horowicz, 1959; Freygang et al., 1964); there is no indication that in muscle it depends on reaction rate. Complete analyses by the model were made with two assumptions about  $P_K$ : (a) it is constant and equals  $1.5 \times 10^{-6}$  cm/sec, a value assumed by Freygang et al. (1964) at  $\phi_s = -84$  mv, and (b) its value is such that all K<sup>+</sup> movement can be ascribed to passive diffusion ( $\nu_K = 0$ ). The question of active K<sup>+</sup> transport was considered in the light of these analyses. In the calculations  $P_{Na} = 0.01 P_K$

and  $P_{Cl} = 3 \times 10^{-6}$  cm/sec (Hodgkin and Horowicz, 1959; Freygang et al., 1964). To obtain  $C_{Cl}^*$ , it first was estimated for the initial and 1 hr conditions by letting  $\phi_{Cl} = \phi_s$  (Hodgkin and Horowicz, 1959).  $(C_{Cl}^*)_{t=0}$  then was calculated by equation 1 *a* when  $\tau = 30$  min, and  $J_{net, Cl}$  was found by equation 1 *b*. Using these values, an improved estimate of  $C_{Cl}^*$  was calculated by equation A 5. Since the new estimated value differed only slightly from the original one, it and  $J_{net, Cl}$  were not recalculated.

The free energy of hydrolysis of ATP,  $\Delta\mu_p$ , was taken as  $-48,000$  joules, using estimated internal concentrations of ATP, adenosine diphosphate (ADP), and  $P_i$  (Kushmerick, 1969). Calculations were done with the use of the GE Mark I time-sharing computer (General Electric Co., Information Devices Dept., Oklahoma City, Okla.).

Fig. 1 represents the flow chart for calculations. Membrane potentials and concentrations were provided in Table I. Changes in concentrations with time were calculated by equation 1 *a* using the time constant  $\tau$  and radius  $r$ , and net ionic fluxes were calculated by equation 1 *b*. With the assumed permeabilities  $P_i^*$  and concentrations  $C_i$  (where \* represents an assumed parameter), the diffusion potential  $\phi_{diff}$ , and  $H$ , the difference between the diffusion potential and  $\phi_s$ , were calculated by equations A 6 and A 7. In addition, ionic passive fluxes due to diffusion and ionic chord conductances  $g_i$  were calculated by equation A 5. Since net ionic flux is the sum of passive and active terms, subtraction of the passive from the net term should give the active term, which is how  $J_{active, K}$  was obtained.  $J_{active, Na}$  was calculated instead by equation 2 for the constraint  $I_{net} = 0$  (see Results). Flux and current are defined as positive in the direction from 1 to 2, i.e., from outside to inside of the cell. Thus,  $J_{active, Na} = -\nu_{Na}J_r$  and  $J_{active, K} = \nu_KJ_r$ , since  $Na^+$  is pumped outward. The ratio

TABLE II  
MEMBRANE POTENTIALS AND IONIC CONCENTRATIONS IN  $Na^+$ -LOADED  
MUSCLES UNDER DIFFERENT CONDITIONS

Condi- tion	$\phi_s$	$C_K^*$	$C_K^*$	$C_{Na}^*$	$C_{Na}^*$	$C_{Cl}^*$	$\phi_K$	$\phi_s - \phi_K$
	mv	moles/liter	moles/liter	moles/liter	moles/liter	moles/liter	mv	mv
A	-76.8	5	88.1	120	31.9	105	-72.3	-4.5
B	-69.9	10	82.7	120	37.2	110	-53.3	-16.6
C	-77	5	65.3	120	54.7	0*	-64.8	-12.2
D	-72.5	10	103.1	120	25	0*	-58.8	-13.7
E	-80	10	95	109.4	52	120.6	-56.7	-23.3
F	-80	10	80	109.4	70	120.6	-52.4	-27.6
G	-80	10	18	109.4	125	120.6	-14.8	-65.2
H	-118	1	92	118.4	45	120.6	-113.9	-4.1
I	-108	2.5	92	116.9	45	120.6	-90.9	-17.1
J	-80	10	92	109.4	45	120.6	-55.9	-24.1
K	-60	25	92	94.4	45	120.6	-32.8	-27.2
L	-25	100	92	19.4	45	120.6	2.1	-27.1

Values in conditions A-D are taken from Harris and Ochs (1966) and are means of more than one muscle pair. The solutions of A and D contained 20 mM  $HCO_3^-$ . The  $C_{Na}^*$  were estimated by assuming  $C_K^* + C_{Na}^* \simeq 120$  mM (cf. Adrian and Slayman, 1966). E-L represent means from Martirosov and Mykaelian (1970). The muscles in E-G had soaked for 24, 48, and 74 hr respectively in  $K^+$ -free solution, which changed the internal ionic concentrations. H-L have different external  $K^+$  (and  $Na^+$ ) concentrations, but internal concentrations are constant.

\* Chloride replaced by methane sulfonate anion.

of active fluxes is the stoichiometric ratio  $\nu_K/\nu_{Na}$ . The constraint  $\nu_K = 0$  means that  $J_{net, K} = J_{passive, K}$ , so that  $P_K$  for this condition was calculated from  $J_{net, K}$ ,  $\phi_s$ , and ionic concentrations by equation A 5.

$Na^+$  efflux kinetics suggest that  $\nu_{Na} = 3$  (Mullins and Frumento, 1963), and a value between 2 and 3 is found in many tissues (Caldwell, 1968), which led us to choose  $\nu_{Na}$  equal to 2 or 3 in the calculations. The model does not require that the  $\nu_i$  be the same for different experimental conditions, and changes in  $\nu_i$  could account for nonlinearities and changes in calculated pump parameters when the experimental conditions changed (see Discussion, equation 3). Reaction rate was calculated from  $-\nu_{Na}J_r$  and compared to the rate of ATP hydrolysis (Dydynska and Harris, 1966). Using the assumed value of  $\Delta\mu_p$ ,  $\Delta F_r$  was calculated by equation A 3 and then  $L_{rr}$  by equation A 2 as the ratio  $J_r/(-\Delta F_r)$ .  $L_{rr}$  was also obtained, as will be shown, from tracer flux measurements and compared with the calculated value. Membrane resistance  $R$ , resistance ratio  $R^o/R$ , and efficiency were calculated by equations A 9-A 11.

In addition to analyzing data of Cross et al. (1965), the relations of  $J_r$ ,  $L_{rr}$ , and  $R$  to ionic concentrations were estimated by the model from data of Martirosov and Mykaelian (1970) (Table II). These authors did two sets of experiments. In conditions E-G of Table II, muscles were left in  $K^+$ -free soaking-in solution for 24, 48, and 72 hr respectively, so as to study membrane potential as a function of internal concentrations. In conditions H-L, outside  $K^+$  was changed with constant internal concentrations. Since conditions E-L are "initial" condition experiments, net ionic fluxes could not be calculated from them. The data of Harris and Ochs (1966) (A-D of Table II) were used to analyze membrane resistance in  $Cl^-$ -containing and  $Cl^-$ -free media, so as to estimate  $P_K$  by equations A 9 and A 10.

## RESULTS

Data of Cross et al. (1965) were analyzed following the flow sheet of Fig. 1, and some calculated means are listed in Table III. Fig. 2 *a* relates  $H = \phi_s - \phi_{diff}$

TABLE III  
CALCULATED MEAN PARAMETERS FOR MUSCLES 1-17 OF TABLE I

Parameters	Units	$P_K = 1.5 \times 10^{-6}$ cm/sec		$P_K$ at $\nu_K = 0^*$
		Initial	1 hr	Initial
$H$	mv	-4.2	-0.6‡	-7.6
$\Delta F_r$	joules $\times 10^3$	-31 (36)§	-20 (29)	-29
$L_{rr}$	moles/sec per $cm^2$ per joule $\times 10^{-16}$	6.0 (7.6)	2.4‡ (0.9)	8.7
$J_r$	pmoles/ $cm^2$ per sec	18.9 (28.4)	1.7 (2.5)	26.2
$FJ_r(\nu_K - \nu_{Na})$	$\mu amp/cm^2$	-1.51	-0.14‡	-7.57
$\nu_K/\nu_{Na}$		0.70	0.83‡	0
$R$	kohm $cm^2$	2.8	2.6	1.2
$R^o/R$		0.99	0.89 (0.96)	0.81
Efficiency		0.4 (0.3)	0.6 (0.4)	0.4

\* Median value of  $P_K$  at  $\nu_K = 0$  is  $6.6 \times 10^{-6}$  cm/sec.

‡ Not significantly different from 0 ( $P > 0.05$ ).

§ Mean within parentheses is for  $\nu_{Na} = 2$  if it differs from mean for  $\nu_{Na} = 3$ , which is outside of parentheses.

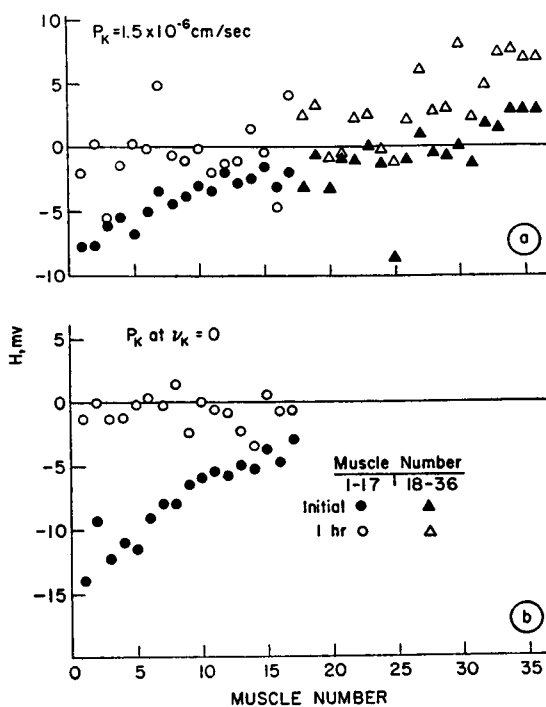


FIGURE 2 Relation of  $H$  to muscle number for  $P_K = 1.5 \times 10^{-6}$  cm/sec and for  $P_K$  at  $\nu_K = 0$ . Results for the latter permeability are shown only for muscles 1-17, when  $\phi_s < \phi_K$  initially. Means of  $H$  are in Table III.

(equation A 7) to muscle number when  $P_K = 1.5 \times 10^{-6}$  cm/sec, where  $\phi_s$  is from Table I and  $\phi_{diff}$  calculated by equation A 6. Most of the muscles appear hyperpolarized initially, although in Table I,  $\phi_s - \phi_K$  may be as positive as +34 mv.  $\phi_s - \phi_K$  as a definition for  $H$  (cf. Kernan, 1962; Cross et al., 1965) was not used because if  $K^+$  is transported actively ( $\nu_K \neq 0$ ) or if the muscle is not at a stationary state,  $K^+$  would not be expected to be in equilibrium with the diffusion potential i.e.,  $\phi_{diff} \neq \phi_K$  (Rapoport, 1970). Fig. 2 *b* shows  $H$  for muscles 1-17 for  $P_K$  at  $\nu_K = 0$ .

The 36 muscles in Table I were rank-ordered and divided into two groups, 1-17 and 18-36. Cross et al. (1965) stated that muscles 3 and 18-36 had been treated with soaking-in solutions containing little or no calcium or had been examined during a cold period which might have damaged the frogs, and usually had membrane potentials more positive than -50 mv in the soaking-in solution. These muscles, whose membrane potentials also were lower than found by Adrian and Slayman (1966), probably were abnormal. For this reason, and because calculated  $J_{passive, Na}$  may be incorrect when  $\phi_s$  is much more positive than -50 mv (see below), results on muscles 18-36 were not tabulated. Inclusion of muscle 3 in the calculations, because of its value of  $\phi_s - \phi_K$ , did not change the results.

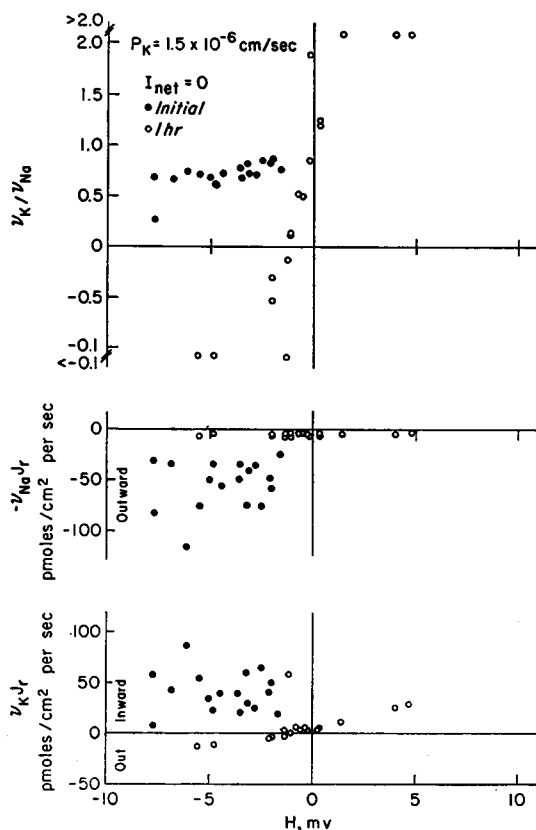


FIGURE 3 Relation for muscles 1-17 of active fluxes and  $\nu_K/\nu_{Na}$  to  $H$ .  $P_K = 1.5 \times 10^{-6}$  cm/sec. Active  $K^+$  flux was calculated as the difference between net  $K^+$  flux (equation 1 *b*) and passive  $K^+$  flux (equations A 4, A 5). Active  $Na^+$  flux was calculated by equation 2 for the constraint  $I_{net} = 0$ .

Since current is not passed across the membrane, the condition  $I_{net} = 0$  always should apply. Calculations did not yield this result when  $J_{net, Na}$  and therefore  $J_{active, Na}$  were found by equation 1 *b*, probably because the mean  $C_{Na}^2$  rather than the individual value for each muscle pair was used in that equation. In the analysis,  $J_{active, Na}$  was calculated instead by the following equation, derived from equation A 4, in which it is first assumed that  $I_{net} = 0$ ,

$$J_{active, Na} = -\nu_{Na} J_r = -\sum_i I_{passive, i} / F - \nu_K J_r. \quad (2)$$

In equation 2, the  $I_{passive, i}$  ( $i = Na^+$ ,  $K^+$ , and  $Cl^-$ ) were calculated by equation A 5 and  $J_{net, K}$  by equation 1 *b* in order to find  $\nu_K J_r$ . The results of the calculation of  $J_{passive, Na}$  are relatively independent of inaccuracies in  $C_{Na}^2$  when  $\phi_s < -50$  mv, because then  $C_{Na}^2$  in equation A 5 is multiplied by a factor  $< 0.14$ .

For  $P_K = 1.5 \times 10^{-6}$  cm/sec, the calculated ionic active fluxes and the stoichi-



ometric ratios of muscles 1-17 are plotted in Fig. 3 for the condition  $I_{\text{net}} = 0$ . Active  $\text{Na}^+$  flux  $-\nu_{\text{Na}}J_r$  is outward and active  $\text{K}^+$  flux  $\nu_{\text{K}}J_r$  is inward initially. At 1 hr, these active fluxes are close to zero.

Table III gives the means of the calculated parameters for muscles 1-17 for the two  $P_{\text{K}}$ 's and  $\nu_{\text{Na}} = 3$  and 2. Many of the 1 hr means for  $P_{\text{K}} = 1.5 \times 10^{-6}$  cm/sec and  $P_{\text{K}}$  at  $\nu_{\text{K}} = 0$  did not differ significantly from zero. Since  $H$  also did not differ from zero, the pump would not contribute to membrane potential according to the model, and the pump parameters cannot be derived from it. A set of 1 hr values is included in Table III for illustrative purposes.

#### *Dependence of Calculated $J_{\text{active, K}}$ on Estimate of $P_{\text{K}}$*

Fig. 4 shows the calculated  $P_{\text{K}}$ 's for muscles 1-17 when  $\text{K}^+$  fluxes were assumed to be due only to passive diffusion ( $\nu_{\text{K}} = 0$ ). The median value of these points is

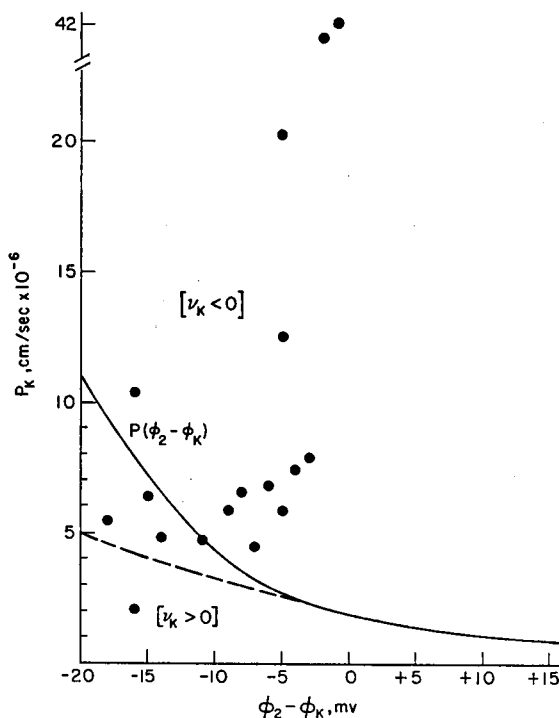


FIGURE 4 Relation of  $P_{\text{K}}$  to  $\phi_2 - \phi_{\text{K}}$ . The solid curve represents our fit to the data of Hodgkin and Horowicz (1959) and is defined as the function  $P(\phi_2 - \phi_{\text{K}})$ . It is extrapolated from their data for  $\phi_2 - \phi_{\text{K}} < -16$  mv, or  $P(\phi_2 - \phi_{\text{K}}) > 8 \times 10^{-6}$  cm/sec to a maximum value of  $15 \times 10^{-6}$  cm/sec. The dashed line represents an alternative fit to the same data (Freygang et al., 1964). The points represent  $P_{\text{K}}$  for muscles 1-17 (Table I) at  $\nu_{\text{K}} = 0$  (no active  $\text{K}^+$  transport). Lower values would fall in the region for which  $\nu_{\text{K}} > 0$  ( $\text{K}^+$  is pumped inward). Higher  $P_{\text{K}}$ 's predict that  $\nu_{\text{K}} < 0$ , which is unlikely (see text). The median value of the points is  $6.6 \times 10^{-6}$  cm/sec. The points overlap the function defined as  $P(\phi_2 - \phi_{\text{K}})$  (continuous line).

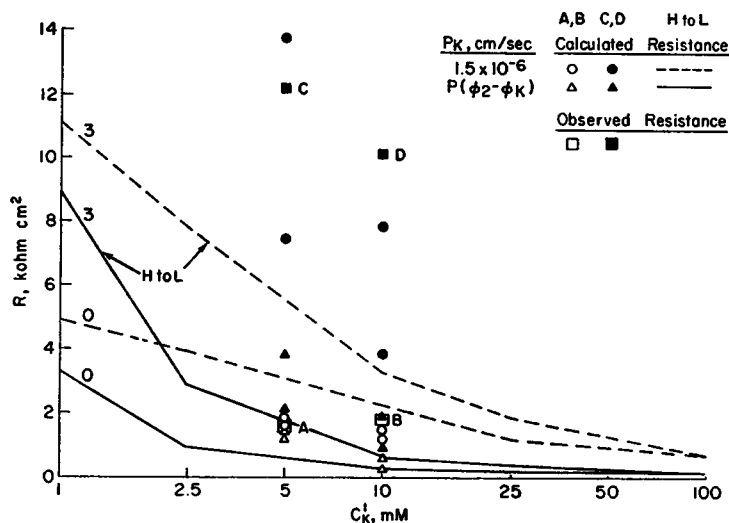


FIGURE 5 Relation of calculated and observed resistances to external  $K^+$ . The lines connect calculated  $R^o$  for H-L, when  $P_K = 1.5 \times 10^{-6}$  cm/sec (dashed lines) and  $P(\phi_2 - \phi_K)$  (continuous lines). For either permeability, the upper line shows  $R^o = R$  (equation A 9) of an electroneutral ( $\nu_{Na} = \nu_K$ ) or absent ( $\nu_{Na} = \nu_K = 0$ ) pump. The lower line shows  $R^o$  when  $\nu_{Na} = 3$  and  $\nu_K = 0$ , as calculated by equations A 9 and A 10. The  $\nu_K$  are the numbers on the left-hand side of the figure. The square symbols are the observed resistances  $R^o$  in conditions A-D.  $P_{O1}$  was taken as  $7 \times 10^{-6}$  cm/sec in A-D (Harris and Ochs, 1966). Pairs of open circles and triangles show calculated  $R^o$  for A and B, pairs of filled circles and triangles for C and D. The upper symbol of each pair gives  $R^o$  for the electroneutral pump, the lower symbol when  $\nu_{Na} = 3$  and  $\nu_K = 0$ .  $P_K$  for A-D appears closer to  $1.5 \times 10^{-6}$  cm/sec than to  $P(\phi_2 - \phi_K)$ .

$6.6 \times 10^{-6}$  cm/sec. If the actual  $P_K$ 's fall below the points in the figure, then the model indicates that  $K^+$  is pumped inward to some degree and that  $\nu_K > 0$ . The region above the points would represent outward  $K^+$  pumping, which is improbable (see Discussion).

Since an accurate estimate of  $P_K$  is unavailable, we will consider several possibilities. The solid line in Fig. 4 represents the function of  $\phi_2 - \phi_K$ , defined as  $P(\phi_2 - \phi_K)$ , which we estimated from data of Hodgkin and Horowicz (1959). It is extrapolated when  $\phi_2 - \phi_K < -16$  mv, and agrees with the curve given by Frumento (1965). The dashed line represents an alternative dependence estimated by Freygang et al. (1964). It is possible that  $P_K$  depends only on membrane potential (Hodgkin and Horowicz, 1959; Freygang et al., 1964), in which case it would have a value less than  $1.5 \times 10^{-6}$  cm/sec for the initial potentials of muscles 1-17.

Fig. 4 shows that  $K^+$  would be expected to be pumped inward initially ( $\nu_K > 0$ ) if  $P_K = 1.5 \times 10^{-6}$  cm/sec, if  $P_K$  is a function of potential alone, or if  $P_K$  is given by the dashed line in the figure. The function  $P(\phi_2 - \phi_K)$  overlaps the points of  $P_K$  for  $\nu_K = 0$ , and represents permeabilities for which  $K^+$  would only move pas-

sively. As expected, the mean  $\nu_K$  calculated with  $P(\phi_s - \phi_K)$  was not significantly different from zero initially for fibers 1-17 ( $P > 0.05$ ).

The measured resistances in conditions A-D can be used to estimate  $P_K$ . Fig. 5 shows that  $P_K$  in these conditions is closer to  $1.5 \times 10^{-6}$  cm/sec than to  $P(\phi_s - \phi_K)$ , which according to the discussion above suggests that  $\nu_K > 0$ . The figure also predicts resistances for conditions H-L, using  $P_K = 1.5 \times 10^{-6}$  cm/sec and  $P(\phi_s - \phi_K)$ . If  $\nu_{Na} = \nu_K$ , the pump is electroneutral and should not affect membrane resistance according to the model. When  $\nu_{Na} = 3$  and  $\nu_K = 0$ , equation A 10 yields a large effect which would make an accurate choice of  $P_K$  difficult, because of the factor  $(\nu_{Na} - \nu_K)^2$  in its denominator (cf. Table III).

#### Relation of Reaction Conductance $L_{rr}$ to Changes in Ionic Concentrations

According to the model and the assumptions of irreversible thermodynamics,  $L_{rr}$  may depend on the parameters of state of the system (concentration, temperature,

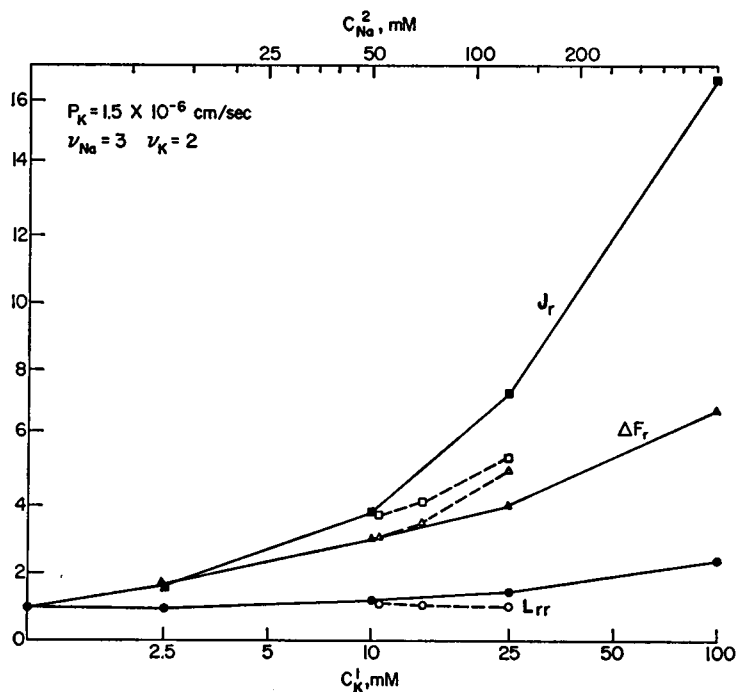


FIGURE 6 Relation of calculated  $J_r$ ,  $L_{rr}$ , and  $\Delta F_r$  to external  $K^+$  and internal  $Na^+$  for conditions E-L of Table I.  $P_K = 1.5 \times 10^{-6}$  cm/sec,  $\nu_{Na} = 3$ ,  $\nu_K = 2$ .  $J_r$ ,  $L_{rr}$ , and  $\Delta F_r$  are scaled to their values at  $C_K^I = 1$  mM (see text). The filled symbols connected by continuous lines represent H-L (varying  $C_K^I$  at  $C_{Na}^I = 45$  mM), and the open symbols connected by dashed lines represent E-G (varying  $C_{Na}^I$  at  $C_K^I = 10$  mM). If  $\nu_K = 0$ ,  $L_{rr}$  and  $J_r$  are multiplied by about one-third and show the same approximate relation to  $C_K^I$  and  $C_{Na}^I$ .

pressure) but should be independent of the reaction rate  $J_r$  and the driving force  $-\Delta F$ , (Rapoport, 1970; Fitts, 1962). While proof of this independence must await an exact understanding of the mechanism of Na-K transport, the relation of  $L_{rr}$  to changes in ionic concentrations can be obtained from the data of this paper. ( $L_{rr}$  was assumed constant for small changes when equations A 10 and 3 (below) were derived).

As pointed out, the data in Table I are insufficient to estimate  $L_{rr}$  at 1 hr because the electrogenic effect of the pump,  $H$ , is insignificant. The change, if any, of  $L_{rr}$  with time should be studied at intervals shorter than 1 hr when  $\phi_s \ll \phi_K$  and  $H \ll 0$ , so that the pump's effect on membrane potential remains sizable and errors in estimating  $\phi_s$  and  $\phi_K$  are relatively unimportant in the calculations.

Conditions E-L of Table II have  $H \ll 0$  and can be used to estimate  $L_{rr}$  for large concentration changes.  $L_{rr}$  was calculated to change much less than  $J_r$  and  $\Delta F$ , for the different assumed  $P_K$ 's and stoichiometries. Fig. 6 is an example of these calculations when  $P_K = 1.5 \times 10^{-6}$  cm/sec,  $\nu_{Na} = 3$ ,  $\nu_K = 2$ . If  $\nu_K = 0$ , equation 3 yields values of  $J_r$  and  $L_{rr}$  which are about three times those in Fig. 6. In the figure,  $J_r$ ,  $L_{rr}$ , and  $\Delta F$ , are scaled to their values at  $C_K^i = 1$  mM (H in Table II), which are, respectively, 9.4 pmoles/cm<sup>2</sup> per sec,  $12.3 \times 10^{-16}$  moles/sec per cm<sup>2</sup> per joule, and -7645 joules. A figure similar to Fig. 6 was obtained for  $P_K = P(\phi_s - \phi_K)$ , but it gave a value of  $J_r$  at  $C_K^i = 10$  mM much larger than  $J_r$  in Table III or when calculated from Na<sup>+</sup> tracer flux or ATP hydrolysis (see below). These calculations suggest that  $P_K$  is closer to  $1.5 \times 10^{-6}$  cm/sec than to  $P(\phi_s - \phi_K)$ .

#### *$L_{rr}$ as Obtained from Na<sup>+</sup> Tracer Efflux*

The relative constancy of  $L_{rr}$  in Fig. 6 for  $C_K^i$  between 1 and 10 mM suggests that, if such is the case,  $J_{\text{active, Na}}$  (equation 15 a of Rapoport, 1970) can be differentiated with respect to  $\ln C_K^i$  when  $L_{rr}$  and  $\nu_i$  are taken as constant, to give

$$\frac{\partial J_{\text{active, Na}}}{\partial \ln C_K^i} = (\nu_{Na} \nu_K - \nu_{Na}^2) FL_{rr} \frac{\partial \phi_s}{\partial \ln C_K^i} - \nu_{Na} \nu_K L_{rr} RT. \quad (3)$$

If  $\partial \phi_s / \partial \phi_K \simeq 1$ , a plot of  $J_{Na} \text{ (tracer) efflux}$  (the change in which is taken as  $J_{\text{active, Na}}$  [Keynes, 1954]) against  $\ln C_K^i$  should be linear with a slope of  $-\nu_{Na}^2 RT L_{rr}$ . Data of Sjodin and Beaugé (1968) when plotted in Fig. 7 for  $C_K^i$  between 1 and 10 mM, give a straight line with a slope of -9.73 pmoles/cm<sup>2</sup> per sec. For  $2 < \nu_{Na} < 3$ , then  $4.4 < L_{rr} < 10.0 \times 10^{-16}$  moles/cm<sup>2</sup> per sec per joule, which agrees with the initial estimates of  $L_{rr}$  in Table III and in Fig. 6. For H-L of Table II, when  $C_K^i$  is between 2.5 and 100 mM,  $\partial \phi_s / \partial \phi_K \simeq 0.85$ , a number which does not modify significantly the estimate of  $L_{rr}$  from Fig. 7.

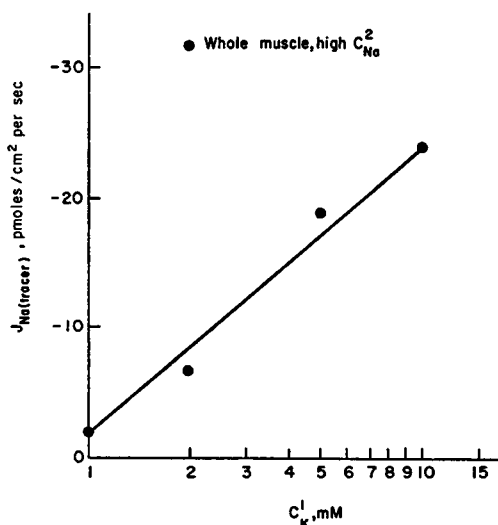


FIGURE 7 Relation of  $J_{Na}(\text{tracer})$  efflux to  $\ln C_K^i$  for  $\text{Na}^+$ -loaded frog sartorius from data of Sjodin and Beaugé (1968). Efflux is defined as a negative flux.

## DISCUSSION

The conclusions of this paper are limited because a complete set of relevant observations to test the model was not made in any experiment. It is suggested that the following measurements should be made on individual muscle pairs:

(a) At any one time,  $C_K^i$ ,  $C_{Na}^i$ ,  $\phi_s$ , and  $R^o$  should be obtained. Cross et al. (1965) did not measure  $R^o$  which can be used to estimate  $P_K$ , nor did they find the individual  $C_{Na}^i$ . The use of a mean,  $\bar{C}_{Na}^i$ , leads to error in calculating  $J_{net, Na}$  by equation 1 b.  $J_{net, Na}$  calculated by equation 1 b can be compared with the value obtained by equation 2 to test the model, if an accurate  $C_{Na}^i$  were known.

(b) The above measurements should be made at two separate times to obtain  $dC_K^i/dt$  and the individual  $J_{net, Na}$  and  $J_{net, K}$ . Time dependence was not studied by Martirosov and Mykaelian (1970), and Harris and Ochs (1966) did not measure  $C_{Na}^i$  with time.

(c) Measurements cited above should be made at different initial  $C_{Na}^i$  and  $C_K^i$  in order to relate  $L_{rr}$  and  $P_K$  to potential, concentration, and time.

The question of whether  $\text{K}^+$  is actively transported ( $\nu_K > 0$ ) could be resolved if an accurate  $P_K$  were known in  $\text{Na}^+$ -loaded muscles. The membrane resistances in conditions A-D, and the  $L_{rr}$  and  $J_r$  as derived with different  $P_K$ 's, suggest that  $P_K$  is closer to  $1.5 \times 10^{-6}$  cm/sec than to  $P(\phi_s - \phi_K)$ . This implies, according to Fig. 4, that  $\text{K}^+$  is transported into the muscle. Active  $\text{K}^+$  transported is also suggested by observations that  $\text{Rb}^+$  and  $\text{Cs}^+$ , like  $\text{K}^+$ , stimulate active  $\text{Na}^+$  efflux, and that both  $\text{Rb}^+$  and  $\text{Cs}^+$  are actively transported into frog muscle (Adrian and Slayman, 1966;

Beaugé and Sjodin, 1968; but see Harris and Ochs, 1966) as well as in rat muscle (Relman et al., 1957).

Geduldig (1968) showed that ouabain, which inhibits the pump, decreases membrane resistance in  $\text{Na}^+$ -loaded muscle, which means that  $R^0/R > 1$  rather than  $< 1$ , as suggested by the model. This discrepancy is important and should be studied further. It could be that ouabain decreases passive resistance, since it increases potassium permeability in rat myometrium (discussed by Taylor et al., 1970), although not in squid axon (Mullins and Brinley, 1969). A way to distinguish  $R^0$  from  $R$  by means other than metabolic inhibition of the pump would be possible if the time for the pump to respond to a step change in membrane potential were longer than the time required to measure instantaneous resistance  $R$ . This would be indicated by a decrease in apparent resistance during the course of application of a current pulse (delayed rectification).

If  $J_r$  in Table III decreases exponentially with the time constant  $\tau = 30$  min, its average value during the first hour in recovery solution is 57% of its initial value, or between 10 and 16 pmoles/cm<sup>2</sup> per sec. Under similar conditions, but with dinitrofluorobenzene in the solution (which inhibits ATP synthesis) muscle ATP is hydrolyzed at a rate of 7.7–18.6 mm/kg per hr (Dydynska and Harris, 1966; Harris, 1967). For  $r = 40 \mu$  and for fiber water = 650 cm<sup>2</sup>/kg wet weight,  $J_r = 6$ –12 pmoles ATP/cm<sup>2</sup> per sec over 1 hr and is within the range given in Table III.  $J_r$  as calculated from  $J_{\text{Na}} (\text{tracer})$  of Fig. 7, for  $\nu_{\text{Na}} = 2$  or 3, is between 8 and 12 pmoles/cm<sup>2</sup> per sec, which also agrees with the above estimates. Thus, the interpretation by the model, that hyperpolarization arises from a reaction-produced current  $FJ_r(\nu_{\text{K}} - \nu_{\text{Na}})$  which flows across the membrane (equation A 7), leads to an estimate of  $J_r$  which agrees with the rate of ATP hydrolysis. It is not necessary to assume that hyperpolarization is caused by  $\text{K}^+$  being pumped into the muscle faster than it is replenished in the extracellular space by diffusion from the bathing solution.

In Fig. 6, calculated  $L_{rr}$  at  $P_{\text{K}} = 1.5 \times 10^{-6}$  cm/sec agrees roughly with the initial  $L_{rr}$  of Table III and with the estimate by equation 3 from tracer flux data. Other tracer data in  $\text{Na}^+$ -loaded muscles cannot be represented by a straight line as in Fig. 7 (Armstrong, 1969), and in unloaded muscles the relation of  $\text{Na}^+$  efflux to external  $\text{K}^+$  depends on  $C'_{\text{Na}}$  (Sjodin, 1970). A nonlinear relation in Fig. 7 would be expected if  $\nu_i$  or  $L_{rr}$  changed with  $C'_{\text{K}}$ , and further experiments in  $\text{Na}^+$ -loaded muscle are required to test this. Nevertheless, agreement among the  $L_{rr}$ 's as obtained from tracer and nontracer observations supports application of the model to  $\text{Na}^+$ -loaded muscle.

In Table III, for  $\nu_{\text{Na}} = 3$ ,  $\Delta F_r = -20,000$  joules at 1 hr, which is close to the 15,500 joules calculated for the red cell at the stationary state when  $\nu_{\text{Na}} = 3$ ,  $\nu_{\text{K}} = 2$  (Garrahan and Glynn, 1967). Net  $\text{Na}^+$  extrusion is expected to take place for  $\Delta F_r < -16,000$  to  $-25,500$  joules as calculated from the "critical energy barrier" of 8370 joules/ $\text{Na}^+$  ion, given by Conway (1960). The efficiency of the pump, estimated to

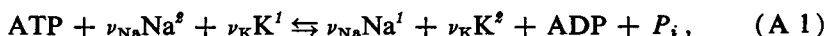
be between 30 and 40% initially (Table III), is comparable to the optimal efficiency of the body as a machine (Brown and Brengelmann, 1965).

Experiments of the type analyzed in this paper give general values for the thermodynamic parameters but say little as regards mechanism. It would be expected that an analysis of deviations about a stationary state would differentiate between linear and nonlinear models. Once this is done, it is expected that the relation between reaction rate and driving force of the reaction, now expressed by equation A 2, can be replaced by a more specific one based upon the mechanism of the active transport pump.

## APPENDIX

### *Summary of Model of Part I (Rapoport, 1970)*

The pump is constituted by the net chemical reaction  $r$  in the active region of the membrane.



where the  $\nu_i$  are net stoichiometric coefficients and the inside of the cell is compartment 2, the outside compartment, 1 (noted by superscripts). The active  $\text{Na}^+$  and  $\text{K}^+$  fluxes are, respectively,  $-\nu_{\text{Na}}J_r$  and  $\nu_{\text{K}}J_r$ , where flux is positive from 1 to 2, and  $J_r$  is the rate of the chemical reaction, moles ATP/cm<sup>2</sup> membrane per sec. We assume that  $J_r$  is a linear function of the free energy change of the net reaction,  $\Delta F_r$ ,

$$J_r = L_{rr}(-\Delta F_r), \quad (\text{A } 2)$$

where  $L_{rr} > 0$  is a conductance coefficient and

$$\Delta F_r = \Delta \bar{\mu}_p + \nu_{\text{K}} RT \ln C_{\text{K}}^{\text{e}}/C_{\text{K}}^{\text{i}} - \nu_{\text{Na}} RT \ln C_{\text{Na}}^{\text{e}}/C_{\text{Na}}^{\text{i}} + (\nu_{\text{K}} - \nu_{\text{Na}}) F \phi_2. \quad (\text{A } 3)$$

$\Delta \bar{\mu}_p$  is the free energy change in the breakdown of ATP,  $F$  is the Faraday,  $\phi_2$  membrane potential.  $\Delta F_r$  depends on membrane potential if  $\nu_{\text{Na}} \neq \nu_{\text{K}}$  because of the last term in equation A 3. The active membrane current  $FJ_r(\nu_{\text{K}} - \nu_{\text{Na}})$  is equal and opposite to the net passive current  $\sum_i g_i(\phi_i - \phi_2)$  when net current is zero:

$$I_{\text{net}} = 0 = \sum_i g_i(\phi_i - \phi_2) + FJ_r(\nu_{\text{K}} - \nu_{\text{Na}}), \quad (\text{A } 4)$$

where the  $g_i$  are the specific ionic conductances and  $\phi_i = z_i RT/F \ln C_i^{\text{i}}/C_i^{\text{e}}$  are the ionic equilibrium potentials. The  $g_i$  can be calculated from  $P_i$  (permeabilities) by use of the constant-field assumption,

$$I_i = g_i(\phi_i - \phi_2) = P_i \frac{F^2 \phi_2 C_i^{\text{e}} \exp(z_i \phi_2 F/RT) - C_i^{\text{i}}}{RT (1 - \exp(z_i \phi_2 F/RT))}. \quad (\text{A } 5)$$

When  $\nu_{\text{K}} \neq \nu_{\text{Na}}$  the pump is electrogenic and the membrane potential differs from the diffusion potential,  $\phi_{\text{diff}}$ , by the quantity  $H$ , where

$$\phi_{\text{diff}} = RT/F \ln \frac{w}{y}, \quad (\text{A } 6)$$

and where

$$w = C_{\text{K}}^{\text{I}} + (P_{\text{Na}}/P_{\text{K}})C_{\text{Na}}^{\text{I}} + (P_{\text{Cl}}/P_{\text{K}})C_{\text{Cl}}^{\text{I}}$$

$$y = C_{\text{K}}^{\text{E}} + (P_{\text{Na}}/P_{\text{K}})C_{\text{Na}}^{\text{E}} + (P_{\text{Cl}}/P_{\text{K}})C_{\text{Cl}}^{\text{E}},$$

$H$  is given by

$$H = \phi_s - \phi_{\text{diff}}$$

$$= \frac{\sum_i g_i \phi_i}{\sum_i g_i} - \phi_{\text{diff}} + \frac{FJ_r(\nu_{\text{K}} - \nu_{\text{Na}})}{\sum_i g_i} \quad (\text{A } 7)$$

as shown by solving for  $\phi_s$  in equation A 4 and substituting in the first expression of equation A 7.

For an electrogenic pump,  $H \neq 0$  and there is a steady-state passive current  $\sum_i g_i(\phi_i - \phi_s)$  given by summing individual ionic currents of equation A 5, where  $w$  and  $y$  are given by equation A 6,

$$I_{\text{passive}} = \frac{F^2 \phi_s P_{\text{K}}}{RT} \frac{w - y \exp(\theta)}{\exp(\theta) - 1}, \quad (\text{A } 8)$$

and where we have inserted the contraction  $\theta = F\phi_s/RT$ . The slope resistance of the passive region of the membrane is  $R = -d\phi_s/dI_{\text{passive}}$ , which is obtained by differentiating equation A 8 with respect to  $\phi_s$ .

$$1/R = \frac{F^2 \phi_s P_{\text{K}} \exp(\theta)}{(RT)^2} \left[ \frac{w - y}{(\exp(\theta) - 1)^2} \right] - \frac{F^2 P_{\text{K}}}{RT} \frac{w - y \exp(\theta)}{\exp(\theta) - 1}. \quad (\text{A } 9)$$

As pointed out in part I, resistance  $R^0$  in the presence of the pump is expected to be less than or equal to resistance  $R$  in its absence, if both are measured at the same membrane potential and ionic concentrations. This inequality will obtain if  $\partial J_r / \partial(-\Delta F_r) \geq 0$ . In order to adjust membrane potential to  $\phi_s$  when the pump is abolished, for the same ionic concentrations and permeabilities a steady-state current equal to the original pump current must be applied across the membrane by a microelectrode. The distinction between this steady microelectrode current and the original pump current is that the former is independent of  $\phi_s$ , while the latter should not be because of the relation of equation A 3 ( $J_r$  depends on  $\phi_s$ ). Once a steady microelectrode current is established, an additional applied current  $dI_{\text{applied}}$  should change membrane potential by  $d\phi_s$  so as to give the resistance  $R$  of equation A 9, as  $dI_{\text{applied}} \rightarrow 0$ . When the pump is not inhibited and produces the steady current which can be changed by membrane potential, the observed resistance is  $R^0 = -d\phi_s/dI_{\text{applied}}$ . When  $L_{rr}$  and  $\nu_i$  are constant, it was shown in part I that

$$\frac{R^0}{R} = \frac{1}{1 + RF^2 L_{rr}(\nu_{\text{Na}} - \nu_{\text{K}})^2} \leq 1. \quad (\text{A } 10)$$



In the absence of a steady pump current (pump absent or electroneutral, where  $\nu_K = \nu_{Na}$ ),  $\phi_{diff} = \phi_s$  and equation A 9 takes a simplified form given by equation 6.0 of Hodgkin and Katz (1949). The efficiency of the pump can be described in terms of membrane potential and stoichiometry, as shown in part I. A general expression for it is,

$$\text{Efficiency} = \frac{-J_{\text{active, Na}}(-\Delta\bar{\mu}_{Na}) - J_{\text{active, K}}(-\Delta\bar{\mu}_K)}{J_r(-\Delta\bar{\mu}_p)}, \quad (\text{A } 11)$$

where  $\Delta\bar{\mu}_i = RT \ln C^i_i/C^e_i + F\phi_s$  for the cations.

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